

VAMUCH Manual for Users*

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1 Introduction

VAMUCH (Variational Asymptotic Method for Unit Cell Homogenization) is a code implementing the various micromechanics theories^{1,2,3,4,5,6,7} based on the variational asymptotic method⁸ to simplify the originally heterogeneous materials using effective homogeneous materials the properties of which are obtained through a micromechanical analysis of a microstructure, commonly called UC (unit cell) or RVE (representative volume element), representative of the heterogeneous material. VAMUCH takes a finite element mesh of the UC including all the details of geometry and material as inputs to calculate the effective properties. These properties are needed for the macroscopic structural analysis to predict the global behavior. The 3D pointwise local field distribution within the microstructure can also be recovered based on the global behavior of the macroscopic structural analysis.

Since most of the theoretical details of VAMUCH are presented in pertinent papers^{1,2,3,4,5,6,7} this manual will only serve to help readers get started using VAMUCH to solve their own micromechanics problems. This manual addresses the history of the code, its features, functionalities, conventions, inputs, outputs, maintenance, and tech support.

2 VAMUCH History

The research project that gave birth to VAMUCH was initiated by Prof. Wenbin Yu in year 2005 under the support of the National Science Foundation (DMI-0522908, 8/01/05-7/31/08) and has been ongoing ever since till the time of writing. The program name VAMUCH first appeared in [9] with its precursor analytical equivalent published in [10]. The original version of VAMUCH, written in Fortran 90/95 was released on January 2006. Many researchers and engineers all over the world are actively using VAMUCH which is becoming a general-purpose micromechanics code.

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3 VAMUCH 2.0 and What is New

VAMUCH was originally designed to run as a stand alone code and its error handling, memory allocation/de-allocation, and I/O were handled with this use in mind. However, in recent years, more and more users began to explore the possibility of using VAMUCH in a design environment. This motivates the major upgrade of VAMUCH to VAMUCH 2.0 through restructuring the code.

As far as the quality of the code concerned, VAMUCH 2.0

1. Is restructured to change the error handling and error message handling, memory allocation and de-allocation, and I/O handling to facilitate its integration with other software environments.
2. Interprets and echoes all the input data for quicker identification of mistakes in the input file).
3. Uses dynamic link libraries (DLLs) to encapsulate the analysis capability so that VAMUCH has true plug-n-play capability which is convenient for integration into other environment. Now VAMUCH can be used both as a standalone application and two callable libraries.
4. Has more thorough and informative error handling.
5. Uses a simplified license mechanism.
6. Has a more detailed manual for end users and a manual for developers.
7. Adopts gfortran as the compiler to create executables for multiple operating systems including Windows, Linux, and Mac.

4 VAMUCH Features

Ref. [11] provides a detailed discussion of the difference between VAMUCH and other common micromechanics approaches. Some of the points are repeating here. If you are not interested in knowing the difference, you can skip this section.

Although it is easy to distinguish VAMUCH from other analytical micromechanics approaches, VAMUCH is often confused as one of the finite element analysis (FEA)-based micromechanics approaches because the equations of the VAMUCH theory are solved using the finite element technique. FEA-based micromechanics approaches carry out a conventional finite element analysis of a UC with specially designed boundary conditions under specifically designed loads. Although VAMUCH has the same versatile modeling capability as FEA-based approaches, VAMUCH is dramatically different from FEA-based approaches, both in its theory and application.

Comparing the corresponding differential statements of VAMUCH and FEA-based approaches, one finds out that that the fundamental variables of VAMUCH are fluctuating functions while those of FEA-based approaches are the macroscopic displacements. Furthermore, the boundary conditions for FEA-based approaches are applied on the macroscopic variables such as displacements. Different sets of displacement boundary conditions are needed for calculating different properties.

Since these boundary conditions are applied a priori based on engineering intuition, it is not surprising that different researchers introduced different boundary conditions for calculating the same property, see [12] for a detailed discussion on the boundary conditions for UCs. It is known that the predicted effective properties are very sensitive to boundary conditions. Another theoretical difference is that the dimensionality of VAMUCH analysis is based on the periodicity of the microstructure. For example, we can use 1D UC to model binary composites, 2D UC to model fiber reinforced composites, and 3D UC to model particle reinforced composites. No special treatment is necessary for these different types of microstructures. However, it is not the case with FEA-based approaches, one has to use 3D UCs to get the complete set of 3D material properties, whether it be a binary composite, fiber reinforced composite, or particle reinforced composite. For example, according to the authors' understanding, Sun and Vaidya¹² derived the most rigorous FEA-based approach for elastic properties, which requires a 3D UC for fiber reinforced composites.

Although there are significant theoretical differences between VAMUCH and other micromechanics approaches, practicing engineers are often more concerned with convenience and efficiency. To this end, we compare VAMUCH and FEA-based approaches. To use a FEA-based approach, one has to carry out multiple runs with different sets of boundary conditions and external loads for predicting different material properties. And postprocessing steps such as averaging stresses or averaging strains are needed for calculating the effective properties. If one is also interested in the local fields within the microstructure, one more run is necessary to predict local stress/strain field if the global stress/strain state is different from that used to obtain the effective properties. Comparing to FEA-based approaches, VAMUCH has the following unique features:

1. VAMUCH can obtain the complete set of material properties within one analysis without applying any load and any boundary conditions, which is far more efficient and less labor intensive than those approaches requiring multiple runs under different boundary and load conditions. It is also noted that VAMUCH can even obtain the complete set of 3D material properties using a one-dimensional analysis of the 1D UC for binary composites. It is impossible for FEA-based approaches.
2. VAMUCH calculates effective properties and local fields directly with the same accuracy as the fluctuating functions. No postprocessing calculations which introduce more approximations, such as averaging stress or strain fields, are needed, which are indispensable for FEM-based approaches.
3. VAMUCH can recover the local fields using a set of algebraic relations obtained in the process of calculating the effective properties. Another analysis of the microstructures which is needed for FEA-based approaches is not necessary for VAMUCH.

Here it is worthwhile to point out that most of these features in VAMUCH application are actually not unique to VAMUCH and are shared by the method of cells (MOC) and its variants developed by Prof. Aboudi and his colleagues. The main difference between VAMUCH and MOC, as far as application is concerned, is that VAMUCH takes full advantage of the finite element technique including versatile discretization capability for arbitrary microstructure, highly efficient linear solvers, and well-developed preprocessing and postprocessing capabilities. An extensive assessment of VAMUCH, MOC and its variants, and FEA-based micromechanics approaches can be found in Ref. [13].

It is also emphasized here that VAMUCH calculations are conceptually different from automating the multiple runs including postprocessing steps of FEA-based approaches using a macro language such as APDL of ANSYS. VAMUCH is not just a different postprocessing approach.

5 VAMUCH Functionalities

VAMUCH is a general purpose micromechanics code and can be used to not only homogenize the heterogeneous materials to obtain effective properties but also to recover the local fields based on the macroscopic information. Specifically, VAMUCH 2.0 has the following functionalities:

1. Carry out an elastic analysis to obtain effective elastic properties of heterogeneous materials and recover the local elastic field.
2. Carry out a heat conduction analysis to obtain effective conductivities of heterogeneous materials and recover the local temperature and heat flux field. Since heat conduction is mathematically analogous to electrostatics, magnetostatics, and diffusion, the present model can also be used to predict effective dielectric, magnetic, and diffusion properties of heterogeneous materials.
3. Carry out thermoelastic analysis to obtain effective thermoelastic properties (including elastic moduli, CTEs, and specific heat) of heterogeneous materials and recover the local elastic field.
4. Carry out multiphysical analysis coupling thermal, mechanical, electric and magnetic effects to obtain effective multiphysical properties and recover the local multiphysic field.

6 VAMUCH Conventions

To understand the inputs and interpret outputs of the program correctly, we need to explain some conventions used by VAMUCH.

First, VAMUCH uses a right hand system, the local coordinate system, denoted as y_1, y_2 and y_3 to describe the microstructure. Depending on the dimensionality of the unit cell, we may not need all the three coordinates. For example for a binary composite made of two different materials alternating along one direction (see Figure 1 for a sketch), The material is uniform along $y_1 - y_2$ plane, and periodic along y_3 direction. The origin of the y_3 is at the geometry center of the unit cell. Because the material is uniform along $y_1 - y_2$ plane, such a microstructure can be meshed by 2-noded 1D elements as showing in Figure 2, where the green circle denotes the corresponding Gauss integration point. Some heterogeneous materials can be modeled using 2D UCs such as the fiber reinforced composites showing in Figure 3, in which the material is uniform along y_1 direction. 2D UCs can be meshed using either triangular elements or quadrilateral elements as showing in Figure 4 and Figure 5, respectively. It is also shown in the figures that VAMUCH numbers the nodes of each 2D elements in the counterclockwise direction. Nodes 1, 2, and 3 of the triangular elements and nodes 1, 2, 3, and 4 of the quadrilateral elements are at the corners. For triangular element, the fourth node is zero to inform VAMUCH that it is a triangular element. Nodes 5, 6, 7 of the triangular elements and nodes 5, 6, 7, 8, 9 for quadrilateral elements are optional nodes.

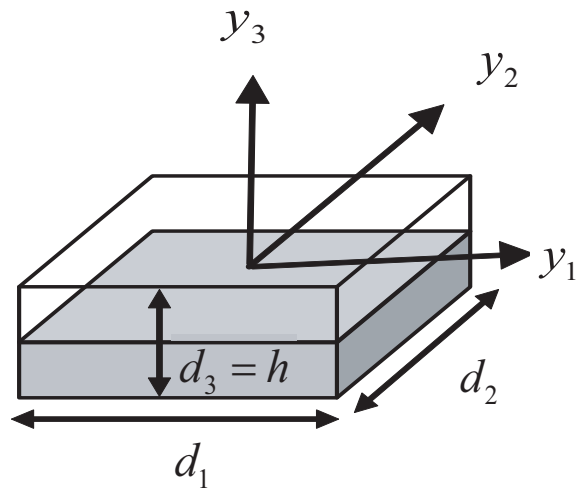


Figure 1: A sketch of binary composite



Figure 2: VAMUCH 1D element numbering and corresponding integration point

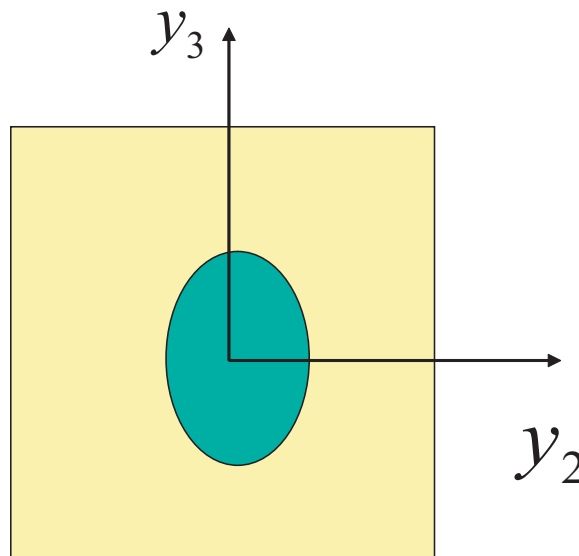


Figure 3: A sketch of fiber reinforced composite

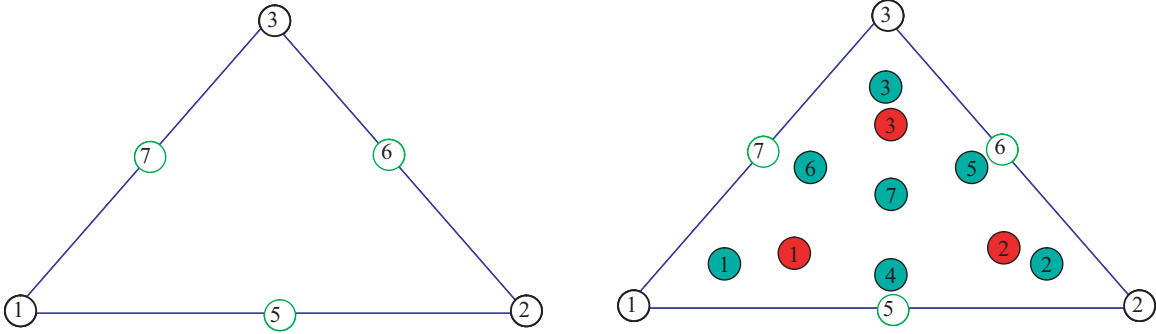


Figure 4: VAMUCH triangular element node numbering and corresponding integration schemes

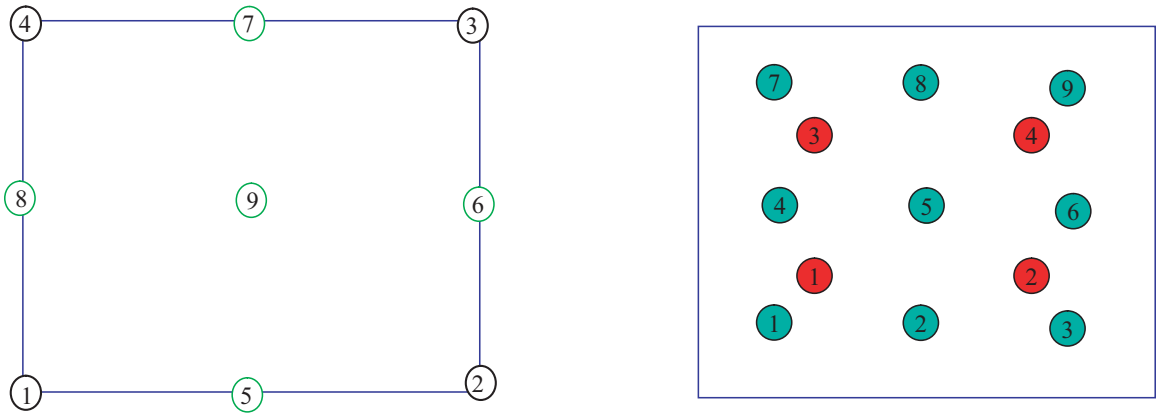


Figure 5: VAMUCH quadrilateral element node numbering and corresponding integration schemes

The red circles denote the Gauss integration points for elements only having corner nodes while the green circles denote the integration points for elements have other nodes in addition to the corner nodes. Some heterogeneous materials should be modeled using 3D UCs such as particle reinforced composites showing in Figure 6, in which all three dimensions along y_1 , y_2 , and y_3 become important. Such UCs can be meshed using either tetrahedral elements or brick elements as showing in Figure 7 and Figure 8, respectively. Note at least the corner nodes should exist and for tetrahedral elements, the fifth node is zero to inform VAMUCH that it is a tetrahedral element. The corresponding integration scheme can be simply generated from their corresponding 2D versions, which can be found in a typical textbook on finite element method. The integration points are not sketched in the figure of 3D elements for simplicity.

In the recovered results, the primary local field such as the displacement field for elastic analysis or the temperature field for heat conduction analysis is reported at each node. However, other fields involving gradients from the primary local field such as stresses and strains are reported at both Gaussian integration point and element nodes, although the values at Gaussian integration points should be considered more accurate.

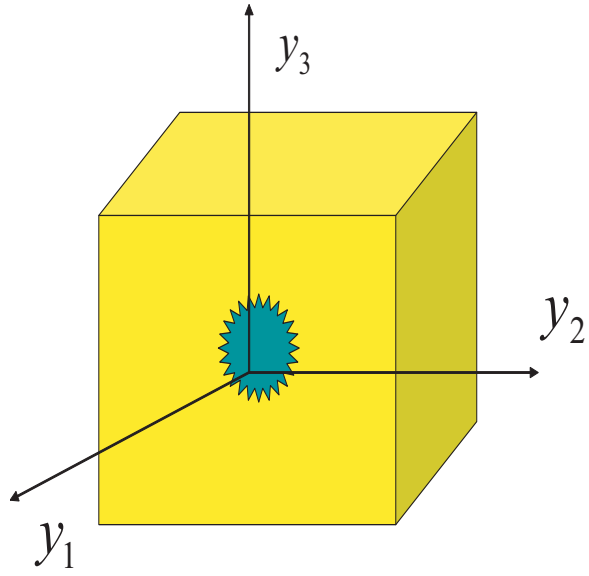


Figure 6: A sketch of particle reinforced composite

7 VAMUCH Inputs

Although general-purpose preprocessors, such as VAMUCH-ANSYS Interface, can be developed to create VAMUCH input files, it is still beneficial for advanced users, particularly those who want to embed VAMUCH in their familiar environment, to understand the meaning of the input data.

The first line has three integers providing the problem control parameters and they are ordered as: “*ndim recover_I analysis*”. *ndim* is an integer number with values 1, 2, or 3 to denote 1D unit cell, 2D unit cell, or 3D unit cell, respectively. *recover_I* is an integer number. If it is 1, VAMUCH will carry out the recovery procedure, otherwise, VAMUCH will carry out constitutive

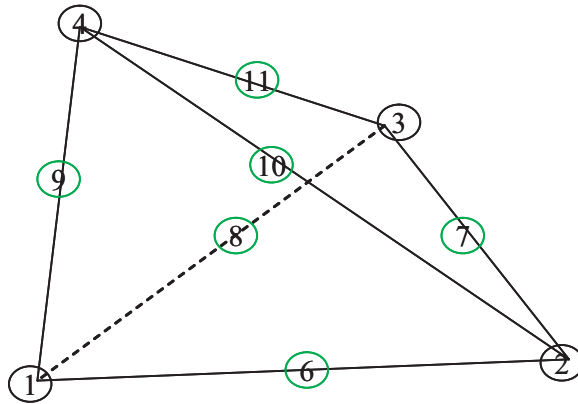


Figure 7: VAMUCH tetrahedral element node numbering

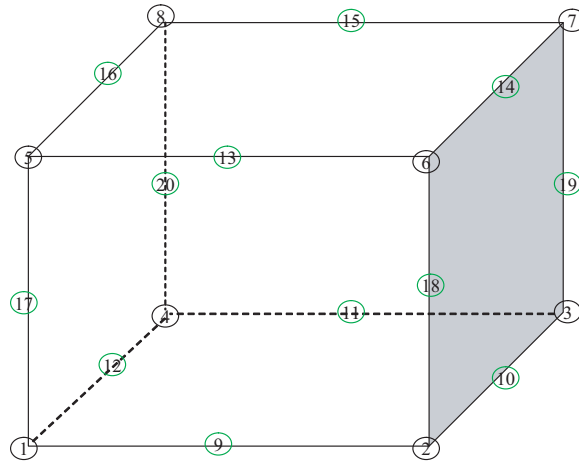


Figure 8: VAMUCH quadrilateral element node numbering

modeling. To recover the local fields, *recover_I* must be 0 first to calculate the effective material properties and fluctuation functions. Additional data for macroscopic fields should be provided at the end of the input file for recovery as specified later. *analysis* is an integer. If it is equal to 0, VAMUCH will carry out elastic analysis; if it is equal to 1, VAMUCH will carry out a thermoelastic analysis; if it is equal to 2, VAMUCH will carry out a conduction analysis. Due to different analysis types, input data could be different as specified in the following.

The next line lists three integers arranged as: “*nnode nelem nmate*,” where *nnode* is the total number of nodes, *nelem* the total number of elements, and *nmate* the total number of material types.

The next *nnode* lines are the coordinates for each node arranged as: “*node_no y1 y2 y3*,” where *node_no* is an integer representing the unique number assigned to each node and y_1, y_2, y_3 are three real numbers describing the location (y_1, y_2, y_3) of the node (only y_3 exists for 1D cells, and y_2 and y_3 exist for 2D cells). **Although the arrangement of *node_no* is not necessary to be consecutive, every node starting from 1 to *nnode* should be present.**

The next *nelem* lines list the nodes for each element (also known as elemental connectivity). They are arranged as: “*elem_no mat_type node_1 node_2 . . .*,” where *elem_no* is the number of element, *mat_type* is an integer to indicate the material type of the element, and *node_i* ($i = 1, 2, \dots$) are nodes belonging to this element. For 1D cells, only two nodes are needed for each element. For 2D cells, nine integers are used for the nodes as an element could have as many as nine nodes. If a node is not present in the element, the value is 0. If the fourth node is zero, it is a triangular element. For 3D cells, 20 integers are used for the nodes as an element could have as many as 20 nodes. If a node is not present in the element, the value is 0. If the fifth node is zero, it is a tetrahedral element; see Figures for the VAMUCH numbering convention. **Although the arrangement of *elem_no* is not necessary to be consecutive, every element starting from 1 to *nelem* should be present.**

The next *nmate* blocks defines the material properties. They are arranged as:

mat_id orth
const1 const2

where *mat_id* is the number of material type, *orth* is the flag to indicate whether the material is isotropic (0), orthotropic (1) or general anisotropic (2). The rest are material constants.

For isotropic materials, *orth* is 0, if *analysis* is 0, there are two constants arranged as:

E ν

where *E* is the Young's modulus and *ν* is the Poisson's ratio. Poisson's ratio must be greater than -1.0 and less than 0.5 for linearly elastic isotropic materials, although VAMUCH allows users to input values that are very close to those limits.

If *analysis* is 1 and *orth* is 0, and there are five constants arranged as:

E ν

α, c_v

T_{ref}

where *α* is the coefficient of thermal expansion, *c_v* is the specific heat, *T_{ref}* is the reference temperature.

If *analysis* is 2 and *orth* is 0, and one only needs to provide on constant:

k

as the thermal conductivity.

For orthotropic materials, *orth* is 1, if *analysis* is 0, there are nine constants arranged as:

E₁ E₂ E₃

G₁₂ G₁₃ G₂₃

ν₁₂ ν₁₃ ν₂₃

including the Young's moduli (*E₁*, *E₂*, and *E₃*), the shear moduli (*G₁₂*, *G₁₃*, and *G₂₃*), and the Poisson's ratios (*ν₁₂*, *ν₁₃*, and *ν₂₃*). The convention of values is such that these values will be used to form the following generalized Hooke's law for composite materials:

$$\begin{Bmatrix} \epsilon_{11} \\ 2\epsilon_{12} \\ \epsilon_{22} \\ 2\epsilon_{13} \\ 2\epsilon_{23} \\ \epsilon_{33} \end{Bmatrix} = \begin{bmatrix} 1/E_1 & 0 & -\nu_{21}/E_2 & 0 & 0 & -\nu_{31}/E_3 \\ 0 & 1/G_{12} & 0 & 0 & 0 & 0 \\ -\nu_{12}/E_1 & 0 & 1/E_2 & 0 & 0 & -\nu_{32}/E_3 \\ 0 & 0 & 0 & 1/G_{13} & 0 & 0 \\ 0 & 0 & 0 & 0 & 1/G_{23} & 0 \\ -\nu_{13}/E_1 & 0 & -\nu_{23}/E_2 & 0 & 0 & 1/E_3 \end{bmatrix} \begin{Bmatrix} \sigma_{11} \\ \sigma_{12} \\ \sigma_{22} \\ \sigma_{13} \\ \sigma_{23} \\ \sigma_{33} \end{Bmatrix}$$

If *analysis* is 1 and *orth* is 1, and there are 14 constants arranged as:

E₁ E₂ E₃

G₁₂ G₁₃ G₂₃

ν₁₂ ν₁₃ ν₂₃

α₁₁ α₂₂ α₃₃ c_v

T_{ref} where *α₁₁*, *α₂₂*, *α₃₃* are the coefficients of thermal expansion along three directions.

If *analysis* is 2 and *orth* is 1, and there are three constants arranged as:

k₁₁ k₂₂ k₃₃

where *k₁₁*, *k₂₂*, *k₃₃* are the thermal conductivities along three directions.

For general anisotropic materials, *orth* is 2, if *analysis* is 0, there are 21 constants arranged as:

$$\begin{array}{cccccc}
 c_{11} & c_{12} & c_{13} & c_{14} & c_{15} & c_{16} \\
 & c_{22} & c_{23} & c_{24} & c_{25} & c_{26} \\
 & & c_{33} & c_{34} & c_{35} & c_{36} \\
 & & & c_{44} & c_{45} & c_{46} \\
 & & & & c_{55} & c_{56} \\
 & & & & & c_{66}
 \end{array}$$

These values are defined using the following generalized Hooke's law:

$$\begin{Bmatrix} \sigma_{11} \\ \sigma_{12} \\ \sigma_{22} \\ \sigma_{13} \\ \sigma_{23} \\ \sigma_{33} \end{Bmatrix} = \begin{bmatrix} c_{11} & c_{12} & c_{13} & c_{14} & c_{15} & c_{16} \\ c_{12} & c_{22} & c_{23} & c_{24} & c_{25} & c_{26} \\ c_{13} & c_{23} & c_{33} & c_{34} & c_{35} & c_{36} \\ c_{14} & c_{24} & c_{34} & c_{44} & c_{45} & c_{46} \\ c_{15} & c_{25} & c_{35} & c_{45} & c_{55} & c_{56} \\ c_{16} & c_{26} & c_{36} & c_{46} & c_{56} & c_{66} \end{bmatrix} \begin{Bmatrix} \epsilon_{11} \\ 2\epsilon_{12} \\ \epsilon_{22} \\ 2\epsilon_{13} \\ 2\epsilon_{23} \\ \epsilon_{33} \end{Bmatrix}$$

If *analysis* is 1 and *orth* is 2, there are 29 constants arranged as:

$$\begin{array}{cccccc}
 c_{11} & c_{12} & c_{13} & c_{14} & c_{15} & c_{16} \\
 & c_{22} & c_{23} & c_{24} & c_{25} & c_{26} \\
 & & c_{33} & c_{34} & c_{35} & c_{36} \\
 & & & c_{44} & c_{45} & c_{46} \\
 & & & & c_{55} & c_{56} \\
 & & & & & c_{66} \\
 \alpha_{11} & 2\alpha_{12} & \alpha_{22} & 2\alpha_{13} & 2\alpha_{23} & \alpha_{33} & c_v
 \end{array}$$

T_{ref}

where α_{ij} , with $i = 1, 2, 3$ and $j = 1, 2, 3$, are the components of the second-order tensor of the thermal expansion coefficients. CTEs corresponding to the shear strains are multiplied by two because the engineering shear strains are twice of the corresponding tensorial shear strains.

If *analysis* is 2 and *orth* is 2, there are six constants arranged as:

$$\begin{array}{ccc}
 k_{11} & k_{12} & k_{13} \\
 & k_{22} & k_{23} \\
 & & k_{33}
 \end{array}$$

where k_{ij} , with $i = 1, 2, 3$ and $j = 1, 2, 3$, are the components of the second-order conductivity tensor.

The material constants are expressed in the local coordinate system y_1, y_2, y_3 . It is also emphasized that if the users are provided material properties in a different coordinate system, or the arrangement of stresses and strains are different from what VAMUCH uses, proper transformation and re-arrangement of the material properties is needed.

Now, we have prepared all the inputs necessary for calculating effective properties, that is, with *recover_I* being 0.

If *recover_I* is 1, the user needs to provide additional information obtained from the macroscopic structural analysis. To carry out recovery, VAMUCH requires the macroscopic primary field (such as temperature for heat conduction or displacement for the elastic analysis) and the gradient of the primary field. For example, If *analysis* is 0 or 1, then the macro displacement and gradient of macro displacements are to be provided to recover the local displacement/strain/stress fields. The data are arranged as:

$$\begin{array}{ccc} v_1 & v_2 & v_3 \\ v_{1,1} & v_{1,2} & v_{1,3} \\ v_{2,1} & v_{2,2} & v_{2,3} \\ v_{3,1} & v_{3,2} & v_{3,3} \end{array}$$

where v_1 , v_2 , and v_3 are the macro displacements and $v_{i,j}$ are the derivatives of macro displacements.

If *analysis=1*, we need to provide an additional data for the macro temperature T .

If *analysis=2*, we need to provide the following four values, arranged as

$$\begin{array}{c} T \\ T_{,1} \quad T_{,2} \quad T_{,3} \end{array}$$

where $T_{,i}$ are the gradient of the macro temperature.

The input file should be ended with a blank line to avoid any possible incompatibility of different computer systems. The input file can be given any name as long as the total number of the characters of the name including extension is not more than 60. You are suggested to use a unique extension say *vam* for you to identify such files with VAMUCH. For the convenience of the user to identify mistakes in the input file, all the inputs are echoed in a file named *input_file_name.ech*. Error messages are also written at the end of *input_file_name.ech*.

8 VAMUCH Outputs

Effective properties obtained by VAMUCH are stored in *input_file_name.K*, including effective stiffness matrix, effective flexibility matrix, and engineering constants if the material can be approximated as orthotropic material. The meaning of the outputs are self explanatory.

The recovered 3D displacement results are stored in *input_file_name.U*. The values are listed for each node identified by its location as: “ $y_2 \ y_3 \ u_1 \ u_2 \ u_3$,” where y_2 and y_3 are the coordinates of the node, u_i the recovered 3D displacements at this node.

The recovered 3D strain/stress results are stored in *input_file_name.ES*. The values are listed for each Gaussian point identified by its location as: “ $y_2 \ y_3 \ \epsilon_{11} \ 2\epsilon_{12} \ \epsilon_{22} \ 2\epsilon_{13} \ 2\epsilon_{23} \ \epsilon_{33} \ \sigma_{11} \ \sigma_{12} \ \sigma_{22} \ \sigma_{13} \ \sigma_{23} \ \sigma_{33}$ ” where ϵ_{ij} and σ_{ij} are the components of the recovered 3D strain tensor and 3D stress tensor, respectively, at the Gaussian point. The recovered 3D strain and stress results at each node are similarly stored in *input_file_name.ESN*.

The average of 3D strain and stress results at Gaussian points for each element are stored in *input_file_name.ELE*, where the integer number indicating the element number, the following six

real numbers are strains, the next six real numbers are the stresses. This set of recovered results can be used to facilitate contour plot for visualization.

All these output files are in pure text format and can be opened by any text editor.

9 VAMUCH Installation

VAMUCH is distributed in the form of VAMUCHx.xReleasePcMM-DD-YEAR.zip for Windows operating systems with “x.x” denotes the version number. Sometimes to circumvent some email systems, the extension “zip” is changed to be “pass”. You just need to change it back to be a zip file once you received it. If you also want to run VAMUCH in other platforms such as Unix/Linux or Mac, please let the author know. Extracting the file VAMUCHx.xReleasePcMM-DD-YEAR.zip to a folder you choose is all you need to do for installation. There are at least three ways to run VAMUCH:

- The safest way to execute VAMUCH is to run *VAMUCH inputfile* as a DOS command in Windows. This can be achieved by Click Start, choose Run, and type in “cmd” and click OK. Then use “cd” to enter the right folder where both the VAMUCH executable and the input file is in.
- Drag your input file into the VAMUCH executable. A window appears to run VAMUCH along with the input file. After it is done, the window will disappear and you have new files generated in the folder of the input file. You can check your results in the output files as described previously.
- Assign a unique extension, say *vam*, to your input file, and configure files with this extension to be opened by VAMUCH and to be edited by a text editor. From a folder’s window, click Tools->Folder Options. Once the Folder Options dialog is open, click tab File Types. Click the New icon to Create New Extension dialog, type *vam* and click OK. With the new file type *vam* highlighted in the Registered file types list, click Advanced to open the Edit File Type dialog. Click Change icon to choose the icon you like. Next, click on New, type *open* under Action, then click Browse and point to the VAMUCH executable and click OK. Click on New, type edit under Action, then click Browse to find the executable for text editor you like to use for editing input files and click OK. Click OK and Close to exit the Folder Options dialog. Then you only need to double click the input file, it will launch VAMUCH for you. You can also rightclick an input file and open it with the text editor.

10 VAMUCH Maintenance and Tech Support

Prof. Yu is committed to maintaining and providing tech support for VAMUCH. A Google group is specifically set up for information exchange related with VAMUCH. *Users are highly encouraged to sign up through <http://groups.google.com/group/hifi-comp> to receive most recent news of VAMUCH, ask questions, and share with others. A technical question should be posted in the Google group before it will be answered.* A page of VAMUCH FAQ will be constantly updated in the group. Before you ask questions, please do the following:

1. Read the VAMUCH manual carefully, if you have not done so;
2. Check the error message at the end of *input_file_name.ech*;
3. Make sure that you have provided the right input data through *input_file_name.ech*, which is VAMUCH's understanding of your input file;
4. Check the VAMUCH FAQ page on the Google group;
5. Post your question in the discussion section of the group.

A web site (hifi-comp.com) has also been created to provide more exposure of the codes Prof. Yu has developed including VABS, VAPAS, VAMUCH, and GEBT through Internet.

11 Epilogue

After a period of continuous development, VAMUCH has reached a level of maturity, and its accuracy has been extensively verified by its developers and users. The performance and robustness of code have been continuously improved based on feedback from its users throughout the world. Although VAMUCH has been designed in such a way that end users do not have to fully understand its theoretical foundation (the details of which are spelled out in VAMUCH related publications), further questions are inevitable because VAMUCH represents a unique micromechanics theory which is drastically different from most conventional micromechanics approaches. Nevertheless, it should be clear that VAMUCH is emerging as a general-purpose micromechanics for engineers to model heterogeneous materials.

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